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Optimizing the Dewatering of Sludge Obtained from Different Treatment Processes along with the Full Scale Application Mahmudul Hasan, Rumana Riffat Department of Civil and Environmental Engineering, The George Washington University

Introduction

The wide application and utilization of the waste activated sludge (WAS) process in the wastewater treatment plant generates a serious disposal problem due to the excess sludge. Many resources have been devoted to reduce the cost of treatment and by decreasing the sludge disposal production, and improving the dewatering process. In most cases, the cost of excess sludge management and handling, including dewatering as well drying and transportation, incineration, comprises a significant fraction of operational costs for the wastewater treatment plants (Mikkelsen and Keilding, 2002).

In this study, dewatering was performed on sludge from different treatment processes. This study will get more comprehensive insights into dewatering mechanisms of different sludge with individual characteristics. Therefore, the inner correlation between sludge characterizations with optimum polymer dose and cake TS% will be investigated. Another focus was be on the role of thermal hydrolysis process (THP) in changing the sludge dewaterability in a mechanistic view. Sludge dewatering also depend on the operational conditions. So the role of operational parameters the on dewatering was also process investigated in this study.

What is Dewatering? It is basically a process of separating the solid waste matter from the sludge and converting into a dried filter cake.

Why Dewatering is necessary?

Dewatering not only saves water but also helps in reducing the amount of waste to be disposed of, reducing the transportation costs, labor, and time.

Methodology Gravity Thickening Samples: 1. Primary sludge Biological Influent 2. WAS sludge activated sludge 3. Mixed sludge (Primary+ Secondary sludge) 4. Thermal-hydrolyzed mixed sludge 5. AD sludge 6. Thermal-hydrolyzed AD sludge Primary Sludge 3-5% TS WAS 3-5% TS Thermal Anaerobic Hydrolysis — 4 Digestion Process Mixed sludge 3-5% TS Thermal-hydrolyzed mixed sludge 11% TS

whole The experiments are divided by two parts. 1. Batch Scale experiment Full scale application

Lab-scale dewatering tests were following the performed methodology described by Higgins et al. (2014) Filtrate were analyzed for Total Suspended Solids (TSS), Volatile Suspended Solids (VSS), total Chemical Oxygen Demand (total COD), particulate COD, colloidal COD, soluble COD, NH3-N, Protein, Polysaccharide and surface charge. The optimum polymer dose range was determined by evaluating the CST.

Sixteen belt filter press dewatering (Winklepress, Ashbrook) have been installed at the Blue Plains facility for a design load of 1000 lbs/m/h and peak load of 1500 lbs/m/h. The Full scale experiments were done for three different operational parameters-Polymer load, belt speed and the Floc mixing rate. Feed and filtrate from the belt filter presses were analyzed for TS, VS, TSS, VSS and ammonium and phosphorus.



Objective

The objectives of the study are mechanistically understanding of dewatering fundamentals on sludge from different treatment processes and investigating the role of operational parameters on sludge dewaterability.





| Type of Sludge | Soluble Protein | Soluble Polysaccharide | Total Bound EPS | Total Surface Charge | Total COD | Soluble COD | NH3-N | Optimum Polymer Dose Cake TS | | Capture Efficiency |
|-----------------------|--------------------|---------------------------|--------------------|-------------------------|------------------|------------------|-----------------|------------------------------|----|-----------------------|
| | (mg/L) | (mg/L) | (mg COD/g VSS) | m eq/gm TS | (mg/L) | (mg/L) | (mg/L) | g Polymer/kg sludge-TS | % | % |
| Primary Sludge | 69±3 | 4±0 | 20.7 | -0.16±0.008 | 75500 ± 707 | $7850\pm\!\!354$ | 147 ± 2.8 | 6.1 | 42 | 99 |
| Secondary Sludge | 167 ± 1 | 102±17 | 404.2 | -0.04±0.014 | 36600±1131 | 320±28 | 89±4 | 5.2 | 15 | 97 |
| Mixed Sludge | 361±3 | 252±1 | 167.5 | -0.19±0.056 | 69500 ± 707 | 7050 ± 71 | 261 ±2.8 | 7.1 | 24 | 97 |
| THP+Supernatent | 7650±49 | 7155±67 | 94.3 | -0.17±0.01 | 86300±1556 | 38650±919 | 740±14 | 10.6 | 45 | 99 |
| AD sludge | 2059±24 | 532±17 | 70.5 | -0.14 ±0.04 | 50650 ± 71 | 5000 ±0 | 2990 ±14.1 | 12 | 32 | 99 |
| Thermal-hydrolyzed AD | 3404±7 | 796±12 | 70.7 | -0.29 ±0.024 | 34000 ± 1414 | 7900 ±424 | 1220 ± 14.1 | 17.2 | 38 | 92 |



The batch scale test proves that sludge composition has a major role in optimum polymer dose and Cake TS.

Optimum polymer dose (OPD) is strongly correlated with soluble protein, and soluble polysaccharide, where THP sludge is the outlier due to the release of excessive amount of protein and polysaccharide. Besides, OPD is moderately correlated with surface charge.

good correlation was found between Cake TS and soluble protein. Primary sludge is an outlier on that graph due to the presence of very low bound EPS.



Conclusion

- The activated \bullet dewaterability, which was due to the high content of bound water within biomass, by comparing the secondary sludge with primary sludge, and thermal-hydrolyzed mixed sludge with THP-AD sludge.
- The improvement in sludge dewatering could be achieved by the thermal hydrolyzed process, for the lysis of the cell and free of the bound water.

Acknowledgement

Funding for this research was provided by the District of Columbia Water and Sewer Authority (DC Water). Special thanks to Haydee De Clippeleir, Ahmed Al-Omari and Qi Zhang.



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sludge has lower

In Fill scale experiment, Cake thickness largely varied for different belt speed. High belt speed (lower loading rate) lower cake causes thickness. But there is no visible change of dewaterability for different floc mixing rate.